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ACCLPTANCE CONTROL CHARTS WITH STIPULATED ERROR PROBABILITIES BASED ON POISSON COUNT DATA.

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Suresh/Matre//
//) Richard L./Scheaffer/**
Richard S./Leavenworth/*

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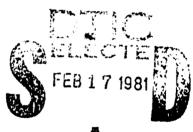
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> *Department of Industrial and Systems Engineering University of Florida Gainesville, Florida 32611

> > **Department of Statistics
> > University of Florida
> > Gainesville, Florida 32611



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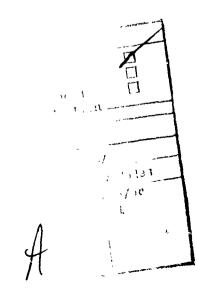
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ACCEPTANCE CONTROL CHARTS WITH STIPULATED ERROR PROBABILITIES BASED ON POISSON COUNT DATA

by

Suresh Mhatre
Richard L. Scheaffer
Richard S. Leavenworth

ABSTRACT

An acceptance control charting scheme is investigated for the case in which observations consist of the number of nonconformances seen when a process is observed for a certain fixed length of time. The counts are assumed to have a Poisson distribution. Two normal approximations for finding the optimum sample size and control limit are compared to the exact values found through the use of Poisson (or Chi-square) probabilities. Recommendations for practical usage are made as a result of a numerical study.

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INTRODUCTION

The application of control chart methods to accept and reject the output of a process has been described in the literature on several occasions. Winterhalter (1945) suggested the use of what he called reject limits in conjunction with the usual control limits to control a process average, \overline{X} . So long as process dispersion was held in control and the control limits lay within the reject limits, virtually all product would meet specifications.

Hill (1956) expanded this idea by employing the reject limits in place of standard control limits for those cases in which the difference between the upper and lower specification limits (U - L) substantially exceeded the natural tolerances of the process, 6 σ '. In his 1957 article, Richard Freund gave more form and substance to Winterhalter's earlier work by providing an analytical basis for deriving the location of a reject limit. He also coined the phrase Acceptance Control Chart and referred to the derived limit as the Acceptance Control Limit (ACL). His development closely follows that for variables acceptance sampling plans. Essentially, it requires the specification of two points on an operating characteristic curve in terms of a quality level and probability of acceptance for each. From these inputs are derived a control limit,

the ACL, and a subgroup size, $\underline{\mathbf{n}}$. So long as the plotted values of $\overline{\mathbf{X}}$ fall within the ACL's, the process may be assumed to be turning out product that meets specifications, subject to the defined risks.

In this paper, we extend Freund's work to the attributes case of counts of nonconformances or nonconformances per unit which can be shown to follow the Poisson distribution. Traditionally, the c-chart has been used when the area of opportunity for a nonconformity to occur is constant; the u-chart has been used when the area of opportunity varies from subgroup to subgroup. Three methods for finding the optimum subgroup size and acceptance control limit are compared. These are: (1) the exact method, employing the Poisson distribution; (2) the standard normal approximation; and (3) the square-root normal transformation.

PROBLEM FORMULATION

Examples include counts of surface imperfections on film, flaws in fabric weave and nonconformities in completed units and subassemblies. The particular application developed in this paper relates to maintenance activities. Frequently maintenance shops process similar types of units, such as hydraulic assemblies, but the units vary substantially in size and time required to process them. In such cases, it may be reasonable to assume that the act of committing an error in processing (the occurence of a nonconformity) has a constant probability as a function of time. The area of opportunity for the occurrence of a nonconformity is thus measured in units of time.

We assume that the quality control procedure consists of observing a process for a length of time, \underline{H} , and counting the number of nonconformances, \underline{X} , that occur during this time interval. We assume that \underline{X}

has a Poisson distribution with intensity λ . That is, the mean number of nonconformances observed in time \underline{H} is $\underline{\lambda}\underline{H}$. Formulating the problem requires the specification of two pairs of values:

- (1) An Acceptable Process Level, λ_0 , and its associated risk level, α . λ_0 is the process quality level that is considered acceptable as a process average measured in terms of nonconformances per 100 worker-hours. The probability of accepting the hypothesis that the process is operating at or below λ_0 , when it actually is operating at λ_0 , is $1-\alpha$.
- (2) A Rejectable Process Level, λ_1 , and its associated risk level, β . λ_1 is the process quality level that is considered unacceptable. The risk of accepting the hypothesis that the process is operating at or below λ_0 when it actually is operating at or above λ_1 is β .

The two points $(\lambda_0, 1-\alpha)$ and (λ_1, β) thus define the operating characteristic curve of the acceptance control chart plan. From these two points we will derive the Acceptance Control Limit, \underline{K} , and the optimal subgroup size, \underline{H} .

Generally speaking, the quality control procedure will involve looking at a series of time intervals, $\underline{\mathbb{H}}_1$, $\underline{\mathbb{H}}_2$, ..., and observing $\underline{\mathbb{X}}_1$, $\underline{\mathbb{X}}_2$, In this case, we assume $\underline{\mathbb{X}}_1$ has a Poisson distribution with mean $\lambda\underline{\mathbb{H}}_1$. $\underline{\mathbb{H}}_1$ can be thought of as the size of the $\underline{\mathbf{I}}^{th}$ subgroup.

The intensity of nonconformances at the acceptable process level (APL) will be deonted by λ_0 , while the intensity at the rejectable process level (RPL) will be denoted by λ_1 . With \underline{K} denoting the acceptance control limit (ACL), we can make the identifications shown in Figure 1.

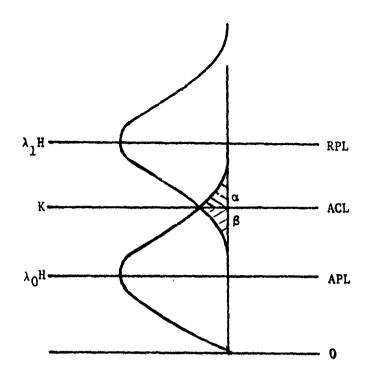


Fig. 1 An Acceptance Control Charting Scheme for Poisson Counts

PROBLEM SOLUTION

Our problem is to determine values of \underline{H} and \underline{K} for fixed values of α , β , λ_0 and λ_1 . Recall that we want to choose \underline{H} and \underline{K} so that the probability of \underline{X} exceeding \underline{K} , when λ_0 is the true intensity, is α ; and the probability of \underline{X} being less than or equal to \underline{K} , when λ_1 is the true intensity, is β .

We shall investigate three methods of calculating \underline{H} and \underline{K} , for fixed λ_0 , λ_1 , α and β . The first will use exact Poisson probabilities; the other two will involve normal approximations to the Poisson. One might ask why approximate procedures are needed when an exact solution is known. The answer lies in the fact that the exact solution, for all possible industrial applications, requires entensive tables of Poisson (or Chi-square) probabilities. Normal approximations have been used in industry and can be worked out quickly and easily with reference to only a table of normal curve areas.

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Exact Solution

We can find the exact solution for \underline{H} and \underline{K} based on Poisson probabilities. If X has a Poisson distribution with mean θ , then

$$P_{\theta}(X \leq C) = P(X_{2(C+1)}^{2} > 2\theta)$$

where $\frac{x^2}{r}$ denotes a Chi-square random variable with \underline{r} degress of freedom. Thus, a table of Chi-square probabilities can be used in place of Poisson probabilities.

Now H and K are found by simultaneously solving the equations

$$P_{\lambda_0 H}(X \le K) = P(X_2^2(K+1) > 2\lambda_0 H) = 1 - \alpha$$

and

$$P_{\lambda_1 H}(X \le K) = P(X_2^2(K + 1) > 2\lambda_1 H) = \beta.$$

These equations must be solved iteratively.

Standard Normal Approximation

If \underline{X} has a Poisson distribution with mean $\underline{\lambda}\underline{H}$, then it is well-known that

$$\frac{X - \lambda H}{\sqrt{\lambda H}}$$

has, approximately, a standard normal distribution if λH is large. (That is, $(X - \lambda H)/\sqrt{\lambda H}$ has a distribution which tends to the standard normal distribution as λH tends to infinity; the approximation seems to work well for λH greater than 5.)

If \underline{z}_{γ} denotes the value that cuts off an upper tail area of γ under the standard normal curve, then \underline{H} and \underline{K} can be found by solving the equations

$$z_{\alpha} = \frac{K - \lambda_0 H}{\sqrt{\lambda_0 H}}$$

and

$$-z_{\beta} = \frac{K - \lambda_{1} H}{\sqrt{\lambda_{1} H}}$$

Solving these equations yields

$$H = \left[\frac{z_{\alpha} \sqrt{\lambda_{o}} + z_{\beta} \sqrt{\lambda_{1}}}{\lambda_{1} - \lambda_{o}} \right]^{2}$$

and

$$K = \lambda_0 H + z_{\alpha} \sqrt{\lambda_0 H} = \lambda_1 H - z_{\beta} \sqrt{\lambda_1 H}$$

Square-Root Normal Transformation

Since \underline{X} , suitably standardized, is approximately normally distributed, it can be shown that $\sqrt{\underline{X}}$ also is approximately normally distributed. The variance of $\sqrt{\underline{X}}$ is essentially free of $\underline{\lambda}$, for large $\underline{\lambda}\underline{H}$, and the distribution of $\sqrt{\underline{X}}$ tends to be more accurately approximated by a normal distribution than does the distribution of \underline{X} , for moderate values of $\underline{\lambda}\underline{H}$.

The second secon

The theory (see Johnson and Kotz [1969]) actually states the $2(\sqrt{X} - \sqrt{\lambda H})$

is approximately distributed as a standard normal random variable if $\underline{\lambda H}$ is large. Working on the true square-root scale, we find \underline{H} and $\overline{\sqrt{\underline{K}}}$ by solving the equations

$$z_{\alpha} = 2(\sqrt{K} - \sqrt{\lambda_0 H})$$

and

$$-z_{\beta} = 2(\sqrt{K} - \sqrt{\lambda_1 H})$$

which yield

$$H = \frac{0.25 \left(z_{\alpha} + z_{\beta}\right)^2}{\left(\sqrt{\lambda_1} - \sqrt{\lambda_0}\right)^2}$$

and

$$\sqrt{K} = \sqrt{\lambda_0 H} + 1/2 z_{\alpha}$$

Transforming back to the original count scale

$$K = (\sqrt{\lambda_0 H} + 1/2 z_{\alpha})^2$$

The equation for \underline{H} is the same as the one in the standard normal case when $\alpha = \beta$.

NUMERICAL STUDY

The values of $\underline{\underline{H}}$ and $\underline{\underline{K}}$ were found for various fixed values of λ_0 , λ_1 , α and β . A representative sample illustrative of our findings is shown in Table 1. The complete set of results is contained in the Appendix. To illustrate these results, we will look at the first row of figures where α = 0.025, β = 0.01, λ_0 = 0.1, and λ_1 = 0.6. We say that the process is out of control if there are more than $\underline{\underline{K}}$ nonconformances in $\underline{\underline{H}}$ time units of observation. $\underline{\underline{K}}$ has the value of 5 for both the standard normal approximation and the exact case and the value 6 for the square-root normal case. Note that the standard normal approximation gives a value of $\underline{\underline{H}}$, 23.469 time units, much larger than the true value, 22.000. Thus we would be observing the process longer than we should, for the same $\underline{\underline{K}}$ value, and, as a result, have a greater probability of seeing more than $\underline{\underline{K}}$ nonconformities than the nominal value of α indicates.

The square-root transformation results in an \underline{H} approximately equal to the true value, but the \underline{K} is slightly larger. Thus the probability of seeing more than \underline{K} nonconformities would be slightly smaller than the nominal value. This pattern prevails throughout most of the cases studied.

TABLE 1 $\begin{tabular}{lll} Values of \underline{H} and \underline{K} for Specified \\ λ_0, λ_1, α and β. \\ \end{tabular}$

 $\alpha = 0.025$

| | | ST ANDAR NORMAL | D | SQUARE RO | ОТ | EXACT (CHI-SQU | ARE) |
|----------------|----------------|--------------------|----|-----------|------|-------------------|------|
| λ ₀ | λ ₁ | н | К | Н | к | Н | К |
| 0.1 | 0.6 | 23.469 | 5 | 21.858 | 6 | 22.000 | 5 |
| 0.2 | 0.7 | 31.887 | 11 | 30.280 | 12 | 31.000 | 11 |
| 0.3 | 0.8 | 39.813 | 18 | 38.222 | 19 | 38.250 | 18 |
| 0.4 | 0.9 | 47.534 | 27 | 45.950 | . 28 | 46.500 | 27 |
| 1.0 | 4.0 | 4.860 | 9 | 4.595 | 10 | 4.795 | 9 |
| 2.0 | 5.0 | 7.067 | 21 | 6.803 | 22 | 6.900 | 21 |
| 3.0 | 6.0 | 9.191 | 37 | 8.927 | 38 | 8.967 | 37 |
| 4.0 | 7.0 | 11.283 | 58 | 11.019 | 58 | 11.172 | 58 |
| | | α = 0.0 |)5 | β = 0.01 | | | |
| 0.1 | 0.6 | 21.578 | 4 | 18.773 | 5 | 19.700 | 4 |
| 0.2 | 0.7 | 28.783 | 9 | 26.005 | 10 | 27.250 | 9 |
| 0.3 | 0.8 | 35.575 | 16 | 32.812 | 16 | 33.500 | 15 |
| 0.4 | 0.9 | 42.195 | 23 | 39.442 | 23 | 39.556 | 22 |
| 1.0 | 4.0 | 4.408 | 7 | 3.944 | 8 | 4.000 | 7 |
| 2.0 | 5.0 | 6.299 | 18 | 5.839 | 18 | 5.860 | 17 |
| 3.0 | 6.0 | 8.131 | 32 | 7.663 | 32 | 7.767 | 31 |
| 4.0 | 7.0 | 9.915 | 50 | 9.459 | 49 | 9.536 | 48 |

TABLE 1, CONT. VALUES OF \underline{H} AND \underline{K} FOR SPECIFIED λ_0 , λ_1 , α and β .

 $\alpha = 0.05$ $\beta = 0.025$

| | | STANDAR NORMAL | | SQUARE NORM | | EXAC (CHI-SQ | |
|----------------|----------------|-------------------|----|----------------|----|-----------------|----|
| ^х 0 | λ ₁ | Н | ĸ | н | K | н | К |
| 0.1 | 0.6 | 16.626 | 3 | 15.469 | 4 | 14.583. | 3 |
| 0.2 | 0.7 | 22.580 | 8 | 21.429 | 8 | 20.570 | 7 |
| 0.3 | 0.8 | 28.186 | 13 | 27.038 | 13 | 28.167 | 13 |
| 0.4 | 0.9 | 33.647 | 19 | 32.501 | 20 | 33.000 | 19 |
| 1.0 | 4.0 | 3.442 | 6 | 3.250 | 7 | 3.285 | 6 |
| 2.0 | 5.0 | 5.003 | 15 | 4.812 | 15 | 4.700 | 14 |
| 3.0 | 6.0 | 6.505 | 26 | 6.314 | 27 | 6.350 | 26 |
| 4.0 | 7.0 | 7.985 | 41 | 7.794 | 41 | 7.988 | 40 |

EXAMPLE APPLICATIONS

Example 1. Check of Repaired Items Against a Standard. The data of Table 2 shows the number of maintenance errors, $\underline{X}_{\underline{1}}$, observed upon sampling repaired aircraft parts for which the actual repair time was $\underline{H}_{\underline{1}}$ hours. In this example, $\underline{H}_{\underline{1}}$ is fixed by the practical sampling circumstances, and so no specific λ_1 needs to be determined. It is desired that λ_0 be 0.01 and α be 0.01. Thus \underline{z}_{α} is 2.33.

TABLE 2 NONCONFORMANCES AMONG REPAIRED ITEMS

| SAMPLE | <u> </u> | H _i | STANDARD NORMAL K | SQUARE ROOT NORMAL K |
|--------|----------|----------------|----------------------|-------------------------|
| 1 | 1 | 58.33 | 2.36 | 3.72 |
| 2 | 4 | 80.22 | 2.89 | 4.24 |
| 3 | 1 | 209.24 | 5.46 | 6.82 |
| 4 | 2 | 164.70 | 4.64 | 5.99 |

Table 2 also shows the values of \underline{K} obtained by the standard normal approximation and the square-root normal transformation. For the first sample:

Standard normal approximation

$$K = \lambda_0 H + z_{\alpha} \sqrt{\lambda_0 H}$$

$$= 0.01(58.33) + 2.33 \sqrt{0.01(58.33)}$$

$$= 2.36$$

Square-root normal transformation

$$K = (\sqrt{\lambda_0 H} + 1/2 z_{\alpha})^2$$

$$= (\sqrt{0.01(58.33)} + 2.33/2)^2$$

$$= 3.72$$

Samples 1, 3 and 4 would be declared "in control" at the standard value of λ_0 under either scheme. However, sample 2, with \underline{X}_2 = 4, would be declared "out-of-control" under the standard normal scheme and "in control" if the square-root normal transformation were used; the observed value is very close to the boundary in either case. Whether we declare the process to be "out-of-control" or "in control" at the point that sample 2 was taken depends upon whether we want to think of the true α risk value as being slightly larger than 0.01 or slightly smaller than 0.01. In many cases declaring a process to be out-of-control when, in fact, it is in control is a costly error. Thus a quality control engineer may wish to use the more conservative procedure that lends itself to smaller α value.

Example 2. Establishing a Standard Plan to Check Maintenance Errors in a Paint Shop. It is desired to set up a standard Acceptance Control Chart plan for checking maintenance errors in an aircraft subassembly paint shop. The acceptable process level is 3 errors per 100 worker-hours with a risk level (α) of 0.05. The rejectable process level is to be 15 errors per 100 worker-hours with a risk level of 0.10. Values of K and H will be found by the three methods.

As previously stated, the Chi-square may be used to solve for Poisson probabilities. Using the Hald Statistical Tables (1952);

$$P(X_{2(K+1)}^{2} \leq 2\lambda_{0}H) = \alpha$$

$$P(X_{2(K+1)}^{2} \leq 2\lambda_{1}H) = 1 - \beta$$

Substituting the values of λ_0 , λ_1 , α , and β into these equations

$$P(X_{2(K+1)}^2 \le 2(0.03)H) = 0.05$$

$$P(X_{2(K+1)}^2 \le 2(0.15)H) = 0.90$$

A convenient search procedure for solving these equations for \underline{K} and \underline{H} is to take the ratios of the values of $\underline{X}^2_{\underline{r}}$ for even values of \underline{r} and solve for the value of \underline{r} that is closest to this ratio. The value of \underline{H} may then be found from the resulting values of $X^2_{\underline{r}}$ taken from the table.

$$\frac{2\lambda_1 H}{2\lambda_0 H} = \lambda_1 / \lambda_0 = 0.15/0.03 = 5.0$$

From the Hald Tables of the Chi-square distribution:

$$\frac{r}{6} = \frac{x^2(r, 0.90)/x^2(r, 0.05)}{10.6 / 1.64 = 6.46}$$

$$8 = 13.4 / 2.73 = 4.91$$

$$10 = 16.0 / 3.94 = 4.06$$

Clearly, the ratio of the two Chi-squares is closest to the desired value of 5.0 when r equals 8. The value of \underline{K} then must be

$$K = (8/2) - 1 = 3$$

H is found by solving the equation

$$2\lambda H = X_{r, \gamma}^2$$

for each (λ, γ) pair and selecting the larger (more conservative value. Thus

$$H = X_{(8, 0.90)}^{2} / 2\lambda_{1} = 13.4 / 2(0.15) = 44.67$$
or
$$H = X_{(8, 0.05)}^{2} / 2\lambda_{0} = 2.73 / 2(0.03) = 45.50$$

Thus our observation time should be 45.50 hours.

In comparison, using the standard normal approximation yields values of H and K of

$$H = \begin{bmatrix} \frac{1.645\sqrt{0.03} + 1.282\sqrt{0.15}}{0.15 - 0.03} \end{bmatrix}^2 = 42.41$$

$$K = 0.03(42.41) + 1.645\sqrt{0.03(42.41)} = 3.13$$

By the square-root normal transformation, these values are

$$H = \frac{0.25(1.645 + 1.282)^2}{(\sqrt{0.15} - \sqrt{0.03})^2} = 46.73$$

$$K = (\sqrt{0.03(46.73)} + 1.645/2)^2 = 4.03$$

It should be noted that the actual values of α and β in this case are 0.040 and 0.122 using the standard normal approximation and 0.014 and 0.172 using the square-root transformation. Thus both approximations are more conservative with respect to α error and less conservative with respect to β error than the plan design called for (α = 0.05 and β = 0.10).

As with many cases involving observations on maintenance operations the actual total maintenance time involved in a sample subgroup is likely to differ from the planned, or design, time. Table 3 shows the actual subgroup times and nonconformities found in 21 subgroups. The actual times range from a low of 32.1 hours to a high of 57.8. This results from the fairly wide discrete time variation required to process a unit. As a consequence, it may be necessary to recompute the control limit based upon the actual time in a subgroup as opposed to the value found for the design time. Since the count of nonconformities is integer-valued, recalculation of the control limit is not always required.

Figure 2 shows the Acceptance Control Chart, using three sets of control limits, for the sampling data of Table 3. Since the actual sample hours vary from subgroup to subgroup, it is inappropriate to plot a central line on this chart. (Where the sample hours can be held constant, a central line would be plotted at $\lambda_0 H$.) The control limit using the exact Poisson is plotted as a dash line at the value 3.5 for all points except subgroups 7, 9, 12, and 21. Recalculation was necessary

Calculation of ACLs and Actual α and β Error Probabilities for Aircraft Maintenance Data TABLE 3.

The State of Contraction

| | | | Ē | Standa | rd Norm | Standard Normal Approximation | imation | Square | -root N | Square-root Normal Transformation | nsformati | uo l |
|----------|-------------------|-------|------------------|--------|---------|-------------------------------|---------|--------|---------|-----------------------------------|-----------|----------|
| | ACL by | | Total noncon- | | | Actual | ual | | | Actual | al | |
| Subgroup | Actual Poisson | Hours | C | × | ACL | ಶ | æ | × | ACL | 8 | 82 | Subgroup |
| | 3.5 | 51.5 | 7 | 3.59 | 3.5 | 0.071 | 0.051 | 4.26 | 4.5 | 0.021 | 0.116 | н |
| 2 | 3.5 | 51.5 | 1 | 3.59 | 3.5 | 0.071 | 0.051 | 4.26 | 4.5 | 0.021 | 0.116 | 2 |
| ٣ | 3.5 | 47.1 | 0 | 3.37 | 3.5 | 0.055 | 0.078 | 4.04 | 4.5 | 0.015 | 0.167 | က |
| 7 | 3.5 | 47.1 | 0 | 3.37 | 3.5 | 0.055 | 0.078 | 4.04 | 4.5 | 0.015 | 0.167 | 4 |
| 5 | 3.5 | 53.1 | 2 | 3.67 | 3.5 | 0.078 | 0.043 | 4.35 | 4.5 | 0.023 | 0.102 | \$ |
| 9 | 3.5 | 7.07 | ٣ | 3.02 | 3.5 | 0.035 | 0.146 | 3.70 | 3.5 | 0.035 | 0.146 | 9 |
| 7 | 4.5 | 57.7 | 0 | 3.90 | 3.5 | 0.098 | 0.027 | 4.57 | 4.5 | 0.032 | 0.068 | 7 |
| 80 | 3.5 | 51.5 | 0 | 3.59 | 3.5 | 0.071 | 0.051 | 4.26 | 4.5 | 0.021 | 0.116 | ∞ |
| 6 | 2.5 | 34.8 | 0 | 2.72 | 2.5 | 0.089 | 0.107 | 3.40 | 3.5 | 0.022 | 0.235 | 6 |
| 10 | 3.5 | 51.5 | П | 3.59 | 3.5 | 0.071 | 0.051 | 4.26 | 4.5 | 0.021 | 0.116 | 10 |
| 11 | 3.5 | 38.8 | П | 2.94 | 2.5 | 0.113 | 0.070 | 3.62 | 3.5 | 0.031 | 0.168 | 11 |
| 12 | 4.5 | 57.8 | ĸ | 3.90 | 3.5 | 0.098 | 0.027 | 4.58 | 4.5 | 0.032 | 0.067 | 12 |
| 13 | 3.5 | 39.1 | 0 | 2.95 | 2.5 | 0.115 | 0.068 | 3.63 | 3.5 | 0.031 | 0.164 | 13 |
| 14 | 3.5 | 49.1 | 2 | 3.47 | 3.5 | 0.062 | 0.065 | 4.15 | 4.5 | 0.017 | 0.142 | 14 |
| 15 | 3.5 | 41.6 | 0 | 3.09 | 3.5 | 0.038 | 0.131 | 3.76 | 3.5 | 0.038 | 0.131 | 15 |
| 16 | 3.5 | 51.5 | 1 | 3.59 | 3.5 | 0.071 | 0.051 | 4.26 | 4.5 | 0.021 | 0.116 | 16 |
| 17 | 3.5 | 42.1 | н | 3.11 | 3.5 | 0.039 | 0.125 | 3.79 | 3.5 | 0.039 | 0.125 | 17 |
| 18 | 3.5 | 54.3 | 2 | 3.73 | 3.5 | 0.083 | 0.038 | 4.41 | 4.5 | 0.025 | 0.092 | 18 |
| 19 | 3.5 | 36.6 | н | 2.82 | 2.5 | 0.099 | 0.089 | 3.50 | 3.5 | 0.026 | 0.203 | 19 |
| 20 | 3.5 | 36.6 | 0 | 2.82 | 2.5 | 0.099 | 0.089 | 3.50 | 3.5 | 0.026 | 0.203 | 20 |
| 21 | 2.5 | 32.1 | 2 | 2.58 | 2.5 | 0.074 | 0.141 | 3.25 | 3.5 | 0.017 | 0.292 | 21 |
| | | | | | | | | | | | | |

for subgroups 7 and 12 (4.5) because of the larger than standard sample hours and for subgroups 9 and 21 because of the smaller than standard sample hours.

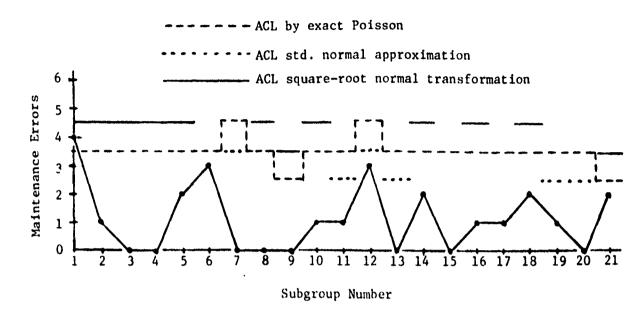


Fig. 2 Acceptance Control Chart for Data of Table 3

Table 3 also shows the values of \underline{K} calculated from the standard normal approximation and from the square-root normal transformation. Again, since the count of nonconformities, \underline{c} , is integer-valued, the ACL for each approximation has been set half-way between integerized values of \underline{K} and $\underline{K}+1$. Where these ACL values differ from those found by the exact Poisson, they are plotted on Figure 2 as dotted lines for the standard normal approximation and as solid lines for the square-root normal transformation.

Observing Figure 2, it should be noted that an out-of-control condition is signalled for subgroup 1 by both the exact Poisson and the standard normal approximation but not by the square-root normal transformation. In those instances wherein the ACL by the standard normal approximation differs from the exact Poisson, it tends to be

(1)

tighter. Thus the standard normal approximation tends to protect more against β error at the sacrifice of α error. The square-root normal transformation tends to act just the opposite. Where it differs from the exact Poisson it tends to be looser affording greater protection against α error at the expense of β error.

This feature is born out by examination of Table 3 in which are tabulated the actual α and β error for each subgroup using each approximation method. Recall that the design level for α was 0.05. By the standard normal approximation, actual α protection ranged from 0.035 to 0.115 with 18 of 21 case above 0.05. In the case of the square-root normal transformation, actual α error ranged from 0.015 to 0.039; all cases were below the design level of 0.05.

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The design level for β was 0.10. In the case of the standard normal approximation, the actual β error ranged from 0.027 to 0.146 with 5 of 21 cases above 0.10. For the square-root transformation all but three cases were above the design level with the actual values ranging from 0.067 to 0.292. In four cases the actual risk levels were more than double the design level.

It should be noted that where the ACL found by an approximation method agrees with that found by the exact Poisson, the true values of α and β apply to the exact Poisson as well. Thus when actual sample hours differ from the value of \underline{H} found from applying the Chi-square formulas, the actual levels of protection may change significantly.

CONCLUSIONS

This paper has described an Acceptance Control Charting approach for process control of cases involving the observation of Poisson counts.

In addition to deliniating a procedure utilizing the exact Poisson,

procedures for use of the popular standard normal approximation and of the not-so-frequently used square-root normal transformation were developed and evaluated.

It was shown that the standard normal approximation tended to favor protection against β error. To the extent that the results of ACL calculations differed from the exact Poisson, the difference was biased in favor of β error protection. On the other hand, usage of the square-root normal transformation leads to ACL calculations offering better protection against α error. To the extent that these calculations differed from the exact Poisson, the bias favored α error protection.

Study of a number of cases, of which Table 1 includes a sample, indicated that the square-root normal transformation gives values of \underline{H} and \underline{K} that oscillate around the true values but that large discrepancies between the approximate and true values are rare. We therefore recommend using the square-root transformation when it is cumbersome or impossible to use exact values and when the cost of α error is high in relation to β error. However, for those cases in which the cost of β error is equal to or greater than that of α error, the standard normal approximation is preferable.

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COMPLETE RESULTS OF NUMERICAL STUDY

 $\alpha = 0.025$

 $\beta = 0.01$

| | | STAND NORM | | SQUARE- NORMA | | ACTU CHI-SO | |
|-----|-----|---------------|-----|------------------|-----|----------------|-----|
| λ0 | λ1 | Н | К | Н | К | Н | К |
| 0,1 | 0.3 | 89.71 | 14 | 85.74 | 15 | 84.83 | 14 |
| 0.2 | 0.4 | 137.86 | 37 | 133.91 | 38 | 134.80 | 37 |
| 0.3 | 0.5 | 184.83 | 70 | 180.88 | 70 | 181.14 | 69 |
| 0.4 | 0.6 | 231.37 | 111 | 227.43 | 111 | 227.71 | 110 |
| 0.5 | 0.7 | 277.71 | 161 | 273.77 | 161 | 273.72 | 160 |
| 0.6 | 0.8 | 323.94 | 221 | 320.00 | 220 | 319.48 | 219 |
| 0.7 | 0.9 | 370.09 | 290 | 366.16 | 289 | 366.29 | 288 |
| 0.8 | 1.0 | 416,20 | 368 | 412.27 | 366 | 411.59 | 365 |
| 0.9 | 1.1 | 462.28 | 456 | 458.35 | 453 | 457.81 | 452 |
| 1.0 | 1.2 | 508.34 | 552 | 504.41 | 549 | 503.83 | 548 |

i = 0.025

F = 0.01

| | | STANDA NORM | | SQUARE- NORM | | ACTU/ CHI-SQI | |
|------|-----|----------------|-----|-----------------|-----|------------------|-----|
| · () | ۱۱ | н | К | Н | К | 11 | К |
| 0.1 | 0.6 | 23.469 | 5 | 21.870 | 6 | 22.000 | 5 |
| 0.2 | 0.7 | 31.887 | 11 | 30.296 | 12 | 31.000 | 11 |
| 0.3 | 0.8 | 39.813 | 18 | 38.226 | 19 | 38.250 | 18 |
| 0.4 | 0.9 | 47.534 | 27 | 45.950 | 28 | 46.500 | 27 |
| 0.5 | 1.0 | 55.145 | 37 | 53.563 | 38 | 53.800 | 37 |
| 0.6 | 1.1 | 62.691 | 49 | 61.110 | 49 | 61.833 | 49 |
| 0.7 | 1.2 | 70.192 | 62 | 68.613 | 63 | 70.087 | 63 |
| 8.0 | 1.3 | 77.665 | 77 | 76.086 | 77 | 76.785 | 77 |
| 0.9 | 1.4 | 85.115 | 93 | 83.537 | 93 | 87.148 | 93 |
| 1.0 | 1.5 | 92.549 | 111 | 90.971 | 111 | 91.991 | 111 |

 $\alpha = 0.025$

 $\beta = 0.01$

| | | STAND NORM | | SQUARE- NORMA | i i | ACTU CHI-SO | |
|------|------|---------------|------|------------------|------|----------------|------|
| λ0 | λ1 | Н | К | Н | К | Н | K |
| 1.0 | 2.0 | 27.57 | 37 | 26.78 | 38 | 26.90 | 37 |
| 2.0 | 3.0 | 46.27 | 111 | 45.49 | 111 | 45.54 | 110 |
| 3.0 | 4.0 | 64.79 | 221 | 64.00 | 220 | 63.90 | 219 |
| 4.0 | 5.0 | 83.24 | 368 | 82.45 | 366 | 82.32 | 365 |
| 5.0 | 6.0 | 101.67 | 552 | 100.88 | 549 | 100.77 | 548 |
| 6.0 | 7.0 | 120.08 | 773 | 119.29 | 769 | 119.23 | 768 |
| 7.0 | 8.0 | 138.48 | 1030 | 137.70 | 1026 | 137.57 | 1024 |
| 8.0 | 9.0 | 156.88 | 1324 | 156.09 | 1319 | 156.07 | 1318 |
| 9.0 | 10.0 | 175.27 | 1655 | 174.49 | 1649 | 174.35 | 1647 |
| 10.0 | 11.0 | 193.67 | 2022 | 192.88 | 2016 | 192.77 | 2014 |

 $\alpha = 0.025$

| | | STAND NORM | | SQUARE- NORM | | ACTU CHI-SQ | |
|------|------|---------------|-----|-----------------|-----|----------------|------------|
| ^O | λ1 | н | K | н | К | Н | К |
| 1.0 | 3.0 | 8.972 | 14 | 8.574 | 15 | 8.483 | 14 |
| 2.0 | 4.0 | 13.786 | 37 | 13.391 | 38 | 13.450 | 3 7 |
| 3.0 | 5.0 | 18.483 | 70 | 18.088 | 70 | 18.114 | 69 |
| 4.0 | 6.0 | 23.137 | 111 | 22.743 | 111 | 22.771 | 110 |
| 5.0 | 7.0 | 27.771 | 161 | 27.377 | 161 | 27.372 | 160 |
| 6.0 | 8.0 | 32.394 | 221 | 32.000 | 220 | 31.948 | 219 |
| 7.0 | 9.0 | 37.009 | 290 | 36.616 | 289 | 36.629 | 288 |
| 8.0 | 10.0 | 41.620 | 368 | 41.227 | 366 | 41.159 | 365 |
| 9.0 | 11.0 | 46.228 | 456 | 45.834 | 453 | 45.781 | 452 |
| 10.0 | 12.0 | 50.834 | 552 | 50.440 | 549 | 50.383 | 548 |

 $\alpha = 0.025$

 $\beta = 0.01$

| | | ST AND NORM | | SQUARE- NORMA | 1 | ACTU | |
|------|------|----------------|-----|------------------|-----|--------|-----|
| λΟ | λ1 | н | К | Н | К | Н | К |
| 1.0 | 4.0 | 4.860 | 9 | 4.595 | 10 | 4.795 | 9 |
| 2.0 | 5.0 | 7.067 | 21 | 6.803 | 22 | 6.900 | 21 |
| 3.0 | 6.0 | 9.191 | 37 | 8.927 | 38 | 8.967 | 37 |
| 4.0 | 7.0 | 11.283 | 58 | 11.019 | 58 | 11.172 | 58 |
| 5.0 | 8.0 | 13.358 | 82 | 13.095 | 82 | 13.176 | 82 |
| 6.0 | 9.0 | 15.425 | 111 | 15.162 | 111 | 15.181 | 110 |
| 7.0 | 10.0 | 17.485 | 144 | 17.223 | 143 | 17.189 | 142 |
| 8.0 | 11.0 | 19.542 | 180 | 19.279 | 180 | 19.304 | 179 |
| 9.0 | 12.0 | 21.596 | 221 | 21.333 | 220 | 21.299 | 219 |
| 10.0 | 13.0 | 23.648 | 266 | 23.385 | 265 | 23.382 | 264 |

 $\alpha = 0.05$

| | | STAND. NORM | | SQUARE- NORM | | ACTU CHI-SQ | |
|-----|-----|----------------|-----|-----------------|-----|----------------|-----|
| ٠0 | λ1 | Н | K | н | К | H | К |
| 0.1 | 0.3 | 80.52 | 12 | 73.6 | 13 | 77.00 | 12 |
| 0.2 | 0.4 | 121.81 | 32 | 114.94 | 32 | 116.50 | 31 |
| 0.3 | 0.5 | 162.10 | 60 | 155.26 | 58 | 156.06 | 58 |
| 0.4 | 0.6 | 202.04 | 95 | 195.22 | 93 | 196.25 | 93 |
| 0.5 | 0.7 | 241.81 | 138 | 235.00 | 136 | 234.58 | 135 |
| 0.6 | 0.8 | 281.49 | 190 | 274.68 | 187 | 274.91 | 186 |
| 0.7 | 0.9 | 321.10 | 249 | 314.30 | 245 | 313.88 | 244 |
| 0.8 | 1.0 | 360.68 | 316 | 353.88 | 311 | 354.23 | 311 |
| 0.9 | 1.1 | 400.23 | 391 | 393.44 | 386 | 393.46 | 385 |
| 1.0 | 1.2 | 439.76 | 474 | 432.97 | 468 | 432.85 | 467 |

 $\alpha = 0.05$

 $\beta = 0.01$

| | | STANDARD NORMAL | | SQUARE-ROOT NORMAL | | ACTUAL CHI-SQUARE | |
|------------|-----|--------------------|----|-----------------------|----|----------------------|----|
| ₹ 0 | λ1 | н | К | Н | K | Н | К |
| 0.1 | 0.6 | 21.578 | 4 | 18.773 | 5 | 19.700 | 4 |
| 0.2 | 0.7 | 28.783 | 9 | 26.005 | 10 | 27.250 | 9 |
| 0.3 | 0.8 | 35.575 | 16 | 32.812 | 16 | 33.500 | 15 |
| 0.4 | 0.9 | 42.195 | 23 | 39.442 | 23 | 39.556 | 22 |
| 0.5 | 1.0 | 48.724 | 32 | 45.977 | 32 | 46.600 | 31 |
| 0.6 | 1.1 | 55.197 | 42 | 52.455 | 41 | 53.250 | 41 |
| 0.7 | 1.2 | 61.633 | 53 | 58.895 | 52 | 59.256 | 52 |
| 0.8 | 1.3 | 68.045 | 66 | 65.310 | 65 | 65.246 | 64 |
| 0.9 | 1.4 | 74.438 | 80 | 71.706 | 78 | 72.032 | 78 |
| 1.0 | 1.5 | 80.817 | 95 | 78.087 | 93 | 78.499 | 93 |

 $\alpha = 0.05$

and a second of the second second

B = 0.01

| | | STANDARD NORMAL | | SQUARE- NORM | | ACTUAL CHI-SQUARE | |
|------|------|--------------------|------|-----------------|------|----------------------|-----------------|
| 70 | λ1 | Н | K | Н | К | Н | К |
| 1.0 | 2.0 | 24.36 | 32 | 22.99 | 32 | 23.30 | 31 |
| 2.0 | 3.0 | 40.41 | 95 | 39.04 | 93 | 39.25 | 93 |
| 3.0 | 4.0 | 56.30 | 190 | 54.94 | 187 | 54.98 | 186 |
| 4.0 | 5.0 | 72.14 | 316 | 70.78 | 311 | 70.85 | 311 |
| 5.0 | 6.0 | 87.95 | 474 | 86.59 | 468 | 86.57 | 467 |
| 6.0 | 7.0 | 103.76 | 663 | 102.40 | 656 | 102.38 | 65 ⁻ |
| 7.0 | 8.0 | 119.55 | 884 | 118.20 | 875 | 118.11 | 874 |
| 8.0 | 9.0 | 135.34 | 1136 | 133.99 | 1126 | 134.03 | 1126 |
| 9.0 | 10.0 | 151.13 | 1420 | 149.77 | 1409 | 149.96 | 1410 |
| 10.0 | 11.0 | 166.92 | 1736 | 165.56 | 1723 | 165.91 | 1726 |

 $\alpha = 0.05$

 $\beta = 0.01$

| | | STANDARD NORMAL | | SQUARE-ROOT NORMAL | | ACTUAL CHI-SQUARE | |
|------|------|--------------------|-----|-----------------------|------|----------------------|-----|
| \0 | λ1 | Н | K | Н | К | Н | К |
| 1.0 | 3.0 | 8.052 | 12 | 7.360 | 13 | 7.700 | 12 |
| 2.0 | 4.0 | 12.181 | 32 | 11.494 | 32 | 12.075 | 32 |
| 3.0 | 5.0 | 16.210 | 60 | 15.526 | ٠ 58 | 15.606 | 58 |
| 4.0 | 6.0 | 20.204 | 95 | 19.522 | 93 | 19.625 | 93 |
| 5.0 | 7.0 | 24.181 | 138 | 23.500 | 136 | 23.458 | 135 |
| 6.0 | 8.0 | 28.149 | 190 | 27.468 | 187 | 27.491 | 186 |
| 7.0 | 9.0 | 32.110 | 249 | 31.430 | 245 | 31.388 | 244 |
| 8.0 | 10.0 | 36.068 | 316 | 35.388 | 311 | 35.423 | 311 |
| 9.0 | 11.0 | 40.023 | 391 | 39.343 | 386 | 39.346 | 385 |
| 10.0 | 12.0 | 43.976 | 474 | 43.296 | 468 | 43.285 | 467 |

 $\alpha = 0.05$

| | | STANDARD NORMAL | | | SQUARE-ROOT NORMAL | | AL UARE |
|------|------|--------------------|-----|--------|-----------------------|--------|------------|
| 10 | λl | Н | К | 11 | К | Н | К |
| 1.0 | 4.0 | 4.408 | 7 | 3.944 | 8 | 4.000 | 7 |
| 2.0 | 5.0 | 6.299 | 18 | 5.839 | 18 | 5.860 | 17 |
| 3.0 | 6.0 | 8.121 | 32 | 7.663 | 32 | 7.767 | 31 |
| 4.0 | 7.0 | 9.915 | 50 | 9.459 | 49 | 9.536 | 48 |
| 5.0 | 8.0 | 11.696 | 71 | 11.241 | 69 | 11.174 | 68 |
| 6.0 | 9.0 | 13.470 | 95 | 13.015 | 93 | 13.083 | 93 |
| 7.0 | 10.0 | 15.238 | 123 | 14.783 | 121 | 14.766 | 120 |
| 8.0 | 11.0 | 17.003 | 155 | 16.549 | 152 | 16.523 | 151 |
| 9.0 | 12.0 | 18.766 | 190 | 18.312 | 187 | 18.327 | 186 |
| 10.0 | 13.0 | 20.527 | 228 | 20.073 | 225 | 20.077 | 224 |

 $\alpha = 0.05$

 $\beta_c = 0.025$

| | | STANDARD NORMAL | | SQUARE-ROOT NORMAL | | ACTUAL CHI-SQUARE | |
|-----|-----|--------------------|-----|-----------------------|-----|----------------------|-----|
| λ0 | λl | н | K | Н | К | Н | K |
| 0.1 | 0.3 | 63.52 | 10 | 60.65 | 11 | 61.5 | 10 |
| 0.2 | 0.4 | 97.58 | 26 | 94.72 | 27 | 95.25 | 26 |
| 0.3 | 0.5 | 130.80 | 49 | 127.94 | 49 | 129.83 | 49 |
| 0.4 | 0.6 | 163.72 | 78 | 160.86 | 78 | 159.99 | 77 |
| 0.5 | 0.7 | 196.49 | 114 | 193.64 | 114 | 193.76 | 113 |
| 0.6 | 0.8 | 229.19 | 156 | 226.64 | 156 | 226.49 | 155 |
| 0.7 | 0.9 | 261.82 | 205 | 258.99 | 204 | 258.54 | 203 |
| 0.8 | 1.0 | 294.45 | 260 | 291.60 | 259 | 291.24 | 258 |
| 0.9 | 1.1 | 327.04 | 322 | 324.20 | 321 | 324.41 | 320 |
| 1.0 | 1.2 | 359.62 | 390 | 356.77 | 389 | 356.99 | 388 |

 $\alpha = 0.05$

| | | STANDARD NORMAL | | SQUARE-ROOT NORMAL | | ACTUAL CHI-SQUARE | |
|-----|-----|--------------------|----|-----------------------|----|----------------------|----|
| 70 | \1 | Н | К | Н | К | 11 | К |
| 0.1 | 0.6 | 16.626 | 3 | 15.469 | 4 | 14.583 | 3 |
| 0.2 | 0.7 | 22.580 | 8 | 21.429 | 8 | 20.571 | 7 |
| 0.3 | 0.8 | 28.186 | 13 | 27.038 | 13 | 28.167 | 13 |
| 0.4 | 0.9 | 33.647 | 19 | 32.601 | 20 | 33.125 | 19 |
| 0.5 | 1.0 | 39.031 | 26 | 37.886 | 27 | 38.100 | 26 |
| 0.6 | 1.1 | 44.368 | 35 | 43.224 | 35 | 43.182 | 34 |
| 0.7 | 1.2 | 49.674 | 44 | 48.531 | 44 | 48.250 | 43 |
| 0.8 | 1.3 | 54.959 | 54 | 53.817 | 55 | 54.068 | 54 |
| 0.9 | 1.4 | 60.229 | 66 | 59.087 | 66 | 59.002 | 65 |
| 1.0 | 1.5 | 65.487 | 78 | 64.345 | 78 | 63.995 | 77 |

u = 0.05

 $\beta = 0.025$

| | | STANDARD NORMAL | | SQUARE-ROOT NORMAL | | ACTUAL CHI-SQUARE | |
|------|------|--------------------|------|-----------------------|------|----------------------|------|
| λΟ | λ1 | н | К | Н | К | Н | ĸ |
| 1.0 | 2.0 | 19.515 | 26 | 18.94 | 27 | 19.05 | 26 |
| 2.0 | 3.0 | 32.743 | 78 | 32.17 | 78 | 32.00 | 77 |
| 3.0 | 4.0 | 45.820 | 156 | 45.27 | 156 | 45.30 | 155 |
| 4.0 | 5.0 | 58.890 | 260 | 58.32 | 259 | 58.25 | 258 |
| 5.0 | 6.0 | 71.923 | 390 | 71.35 | 389 | 71.40 | 388 |
| 6.0 | 7.0 | 84.946 | 546 | 84.38 | 544 | 84.34 | 543 |
| 7.0 | 8.0 | 97.960 | 728 | 97.40 | 725 | 97.31 | 724 |
| 8.0 | 9.0 | 110.980 | 936 | 110.41 | 933 | 110.40 | 932 |
| 9.0 | 10.0 | 123.990 | 1170 | 123.42 | 1166 | 123.36 | 1165 |
| 10.0 | 11.0 | 136.990 | 1430 | 136.43 | 1426 | 136.34 | 1424 |

 $\tau = 0.05$

| | | STANDARD NORMAL | | SQUARE- NORM | i | ACTUAL CHI-SQUARE | |
|------|------|--------------------|-----|-----------------|-----|----------------------|-----|
| () | λ1 | Н | K | Н | К | H | К |
| 1.0 | 3.0 | 6.352 | 10 | 6.063 | 11 | 6.150 | 10 |
| 2.0 | 4.0 | 9.758 | 26 | 9.471 | 27 | 9.525 | 26 |
| 3.0 | 5.0 | 13.080 | 49 | 12.794 | 49 | 12.679 | 48 |
| 4.0 | 6.0 | 16.372 | 78 | 16.086 | 78 | 15.999 | 77 |
| 5.0 | 7.0 | 19.649 | 114 | 19.364 | 114 | 19.376 | 113 |
| 6.0 | 8.0 | 22.919 | 156 | 22.634 | 156 | 22.650 | 155 |
| 7.0 | 9.0 | 26.184 | 205 | 25.899 | 204 | 25.854 | 203 |
| 8.0 | 10.0 | 29.445 | 260 | 29.160 | 259 | 29.124 | 258 |
| 9.0 | 11.0 | 32.704 | 322 | 32.419 | 321 | 32.441 | 320 |
| 10.0 | 12.0 | 35.962 | 390 | 35.677 | 389 | 35.699 | 388 |

 $\alpha = 0.05$

 $\beta = 0.025$

| | | STANDARD NORMAL | | | SQUARE-ROOT NORMAL | | AL QUARE |
|------|------|--------------------|-----|--------|-----------------------|--------|--------------------|
| \() | λ1 | Н | К | 11 | К | Н | K |
| 1.0 | 4.0 | 3.442 | 6 | 3.250 | 7 | 3.285 | 6 |
| 2.0 | 5.0 | 5.003 | 15 | 4.812 | 15 | 4.700 | 14 |
| 3.0 | 6.0 | 6.505 | 26 | 6.314 | 27 | 6.350 | 26 |
| 4.0 | 7.0 | 7.985 | 41 | 7.794 | 41 | 7.779 | 40 |
| 5.0 | 8.0 | 9.453 | 58 | 9.262 | 58 | 9.364 | 58 |
| 6.0 | 9.0 | 10.914 | 78 | 10.724 | 78 | 10.666 | 77 |
| 7.0 | 10.0 | 12.372 | 101 | 12.182 | 101 | 12.138 | 100 |
| 8.0 | 11.0 | 13.827 | 127 | 13.637 | 127 | 13.616 | 126 |
| 9.0 | 12.0 | 15.279 | 156 | 15.089 | 156 | 15.100 | 155 |
| 10.0 | 13.0 | 16.731 | 188 | 16.541 | 187 | 16.500 | 186 |

 $\alpha = 0.01$

| | | ST ANDARD NORMAL | | , , | SQUARE-ROOT NORMAL | | AL UARE |
|------|-----|---------------------|-----|--------|-----------------------|--------|------------|
| 7 () | ۱۱ | н | К | Н | К | Н | К |
| 0.1 | 0.3 | 81.86 | 14 | 85.74 | 17 | 82.50 | 15 |
| 0.2 | 0.4 | 130.01 | 37 | 133.91 | 40 | 133.75 | 39 |
| 0.3 | 0.5 | 176.98 | 70 | 180.88 | 73 | 180.88 | 72 |
| 0.4 | 0.6 | 223.52 | 111 | 227.43 | 115 | 227.97 | 114 |
| 0.5 | 0.7 | 269.86 | 161 | 273.77 | 165 | 274.31 | 165 |
| 0.6 | 0.8 | 316.08 | 221 | 319.99 | 226 | 320.26 | 225 |
| 0.7 | 0.9 | 362.24 | 290 | 366.16 | 295 | 365.96 | 294 |
| 0.8 | 1.0 | 408.35 | 368 | 412.27 | 373 | 411.55 | 372 |
| 0.9 | 1.1 | 454.43 | 456 | 458.35 | 461 | 457.98 | 460 |
| 1.0 | 1.2 | 500.48 | 552 | 504.41 | 558 | 504.17 | 557 |

 $\alpha = 0.01$

 $\beta = 0.025$

| | | STANDARD NORMAL | | , ' | SQUARE-ROOT NORMAL | | AL QUARE |
|-----|-----|--------------------|-----|--------|-----------------------|--------|--------------------|
| 70 | λ1 | Н | K | Н | К | Н | К |
| 0.1 | 0.6 | 20.328 | 5 | 21.870 | 7 | 23.300 | 6 |
| 0.2 | 0.7 | 28.746 | 11 | 30.296 | 13 | 30.500 | 12 |
| 0.3 | 0.8 | 36.672 | 18 | 38.226 | 21 | 37.000 | 19 |
| 0.4 | 0.9 | 44.392 | 27 | 35.950 | 30 | 44.944 | 28 |
| 0.5 | 1.0 | 52.004 | 37 | 53.563 | 40 | 53.500 | 39 |
| 0.6 | 1.1 | 59.549 | 49 | 61.110 | 52 | 60.736 | 51 |
| 0.7 | 1.2 | 67.051 | 62 | 68.613 | 66 | 68.917 | 65 |
| 0.8 | 1.3 | 74.523 | 77 | 76.086 | 80 | 76.501 | 80 |
| 0.9 | 1.4 | 81.973 | 93 | 83.537 | 97 | 83.582 | 96 |
| 1.0 | 1.5 | 89.407 | 111 | 90.971 | 115 | 91.186 | 114 |

 $\alpha = 0.01$

| | | STANDARD NORMAL | | , | SQUARE-ROOT NORMAL | | AL UARE |
|------|------|--------------------|------|--------|-----------------------|--------|------------|
| .0 | λ1 | Н | K | Н | K | Н | К |
| 1.0 | 2.0 | 26.00 | 37 | 26.78 | 40 | 26.75 | 39 |
| 2.0 | 3.0 | 44.70 | 111 | 45.49 | 115 | 45.59 | 114 |
| 3.0 | 4.0 | 63.22 | 221 | 64.00 | 226 | 64.05 | 225 |
| 4.0 | 5.0 | 81.67 | 368 | 82.45 | 373 | 82.31 | 372 |
| 5.0 | 6.0 | 100.10 | 552 | 100.88 | 558 | 100.83 | 557 |
| 6.0 | 7.0 | 118.51 | 773 | 119.29 | 779 | 119.20 | 778 |
| 7.0 | 8.0 | 136.92 | 1030 | 137.70 | 1037 | 137.60 | 1036 |
| 8.0 | 9.0 | 155.31 | 1324 | 156.10 | 1332 | 156.03 | 1331 |
| 9.0 | 10.0 | 173.70 | 1655 | 174.48 | 1664 | 174.36 | 1662 |
| 10.0 | 11.0 | 192.10 | 2022 | 192.88 | 2032 | 192.73 | 2030 |

 $\alpha = 0.01$

 $\beta = 0.025$

| | λ1 | STANDARD NORMAL | | SQUARE-ROOT NORMAL | | ACTUAL CHI-SQUARE | |
|------|------|--------------------|-----|-----------------------|-----|----------------------|-----|
| λΟ | | н | K | Н | K | Н | K |
| 1.0 | 3.0 | 8.186 | 14 | 8.574 | 17 | 8.250 | 15 |
| 2.0 | 4.0 | 13.001 | 37 | 13.391 | 40 | 13.375 | 39 |
| 3.0 | 5.0 | 17.697 | 70 | 18.088 | 73 | 18.088 | 72 |
| 4.0 | 6.0 | 22.353 | 111 | 22.743 | 115 | 22.797 | 114 |
| 5.0 | 7.0 | 26.986 | 161 | 27.377 | 165 | 27.431 | 165 |
| 6.0 | 8.0 | 31.608 | 221 | 32.000 | 226 | 32.026 | 225 |
| 7.0 | 9.0 | 36.224 | 290 | 36.616 | 295 | 36.596 | 294 |
| 8.0 | 10.0 | 40.835 | 368 | 41.227 | 373 | 41.155 | 372 |
| 9.0 | 11.0 | 45.443 | 456 | 45.834 | 461 | 45.789 | 460 |
| 10.0 | 12.0 | 50.048 | 552 | 50.440 | 558 | 50.417 | 557 |

 $\alpha = 0.01$

| | λι | STANDARD NORMAL | | SQUARE-ROUT NORMAL | | ACTUAL CHI-SQUARE | |
|------|------|--------------------|-----|-----------------------|-----|----------------------|-----|
| 0 | | Н | К | н | К | Н | K |
| 1.0 | 4.0 | 4.337 | 9 | 4.595 | 11 | 4.275 | 9 |
| 2.0 | 5.0 | 6.544 | 21 | 6.803 | 24 | 6.675 | 22 |
| 3.0 | 6.0 | 8.667 | 37 | 8.927 | 40 | 10.550 | 39 |
| 4.0 | 7.0 | 10.759 | 58 | 11.019 | 61 | 10.998 | 60 |
| 5.0 | 8.0 | 12.835 | 82 | 13.095 | 86 | 13.113 | 85 |
| 6.0 | 9.0 | 14.901 | 111 | 15.162 | 115 | 15.198 | 114 |
| 7.0 | 10.0 | 1 962 | 144 | 17.223 | 147 | 17.261 | 147 |
| 8.0 | 11.0 | 19.018 | 180 | 19.279 | 184 | 19.311 | 184 |
| 9.0 | 12.0 | 21.072 | 221 | 21.333 | 226 | 21.351 | 225 |
| 10.0 | 13.0 | 23.124 | 266 | 23.385 | 271 | 23.383 | 270 |